

# A smaller global estimate of the second indirect aerosol effect

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[1] Global estimates of the indirect aerosol effect much larger than  $1 \text{ W m}^{-2}$  in magnitude are difficult to reconcile with observations, yet climate models give estimates between  $-1$  and  $-4.4 \text{ W m}^{-2}$ . We use a climate model with a new treatment of autoconversion to reevaluate the second indirect aerosol effect. We obtain a global-mean value of  $-0.28 \text{ W m}^{-2}$ , compared to  $-0.71 \text{ W m}^{-2}$  with the autoconversion treatment most often used in climate models. The difference is due to (1) the new scheme's smaller autoconversion rate, and (2) an autoconversion threshold that increases more slowly with cloud droplet concentration. The impact of the smaller autoconversion rate shows the importance of accurately modeling this process. Our estimate of the total indirect aerosol effect on liquid-water clouds changes from  $-1.63$  to  $-1.09 \text{ W m}^{-2}$ .

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## 1. Introduction

[2] The most uncertain of the anthropogenic climate forcings are the indirect aerosol effects on clouds. Estimates for the first indirect effect, whereby an increase in aerosols leads to a decrease in cloud-droplet effective radius and hence an increase in cloud albedo, range from 0 to  $-2 \text{ W m}^{-2}$  according to *Intergovernmental Panel on Climate Change (IPCC)* [2001a, 2001b]. The second indirect aerosol effect, whereby smaller droplets in polluted clouds form raindrops less efficiently, was considered too uncertain to be included in the IPCC's estimates. Simulations using global climate models (GCMs) suggest that the second indirect effect should enhance the first indirect effect, by increasing cloud liquid-water path [IPCC, 2001b]. Estimates in the range of  $-1$  to  $-4.4 \text{ W m}^{-2}$  for the combined indirect effect have been obtained in recent GCMs [Ghan et al., 2001; Jones et al., 2001; Lohmann and Feichter, 2001; Kristjánsson, 2002; Menon et al., 2002; Suzuki et al., 2004]. However, such large estimates are difficult to reconcile with observed temperature records [Anderson et al., 2003]. Furthermore, a general increase of cloud liquid-water path with increased aerosol loading, as predicted by GCM simulations, has not been found in recent empirical studies [e.g., Han et al., 2002].

[3] These discrepancies between GCMs and observations suggest that indirect aerosol effects may be overestimated in GCMs [Lohmann and Lesins, 2002]. A partial explanation was offered by Liu and Daum [2002], who showed that

increases in cloud droplet concentration are associated with increased dispersion (breadth) of the cloud droplet size distribution, and that the increased dispersion counteracts the first indirect aerosol effect. Subsequent GCM simulations have confirmed that neglect of the dispersion effect can lead to overestimation of the first indirect aerosol effect [Peng and Lohmann, 2003; Rotstajn and Liu, 2003].

[4] It is also expected from cloud physics theory [Beard and Ochs, 1993] that increased dispersion will enhance the coalescence of cloud droplets (autoconversion) and thereby offset the second indirect effect, but this has been ignored in GCMs. In this paper, we present new GCM-based calculations of the second indirect effect using a new autoconversion scheme, which accounts for the dispersion effect. We also recalculate the second indirect effect using the autoconversion scheme that has been most widely used in GCMs, and explain the reasons for the smaller result obtained with the new scheme.

## 2. Autoconversion Parameterizations

[5] The autoconversion parameterization ("R<sub>3</sub> scheme") most widely used in GCM simulations of the second indirect effect [Rotstajn, 2000; Ghan et al., 2001; Jones et al., 2001; Kristjánsson, 2002; Menon et al., 2002] can be expressed as [Baker, 1993; Boucher et al., 1995]

$$P = E_c \pi \kappa_1 \left( \frac{3}{4\pi\rho_l} \right)^{4/3} N^{-1/3} L^{7/3} H(R_3 - R_{3c}), \quad (1)$$

where  $P$  is the rate of decrease of liquid-water content due to autoconversion,  $E_c$  is a constant collection efficiency,  $\kappa_1 = 1.19 \times 10^6 \text{ cm}^{-1} \text{ s}^{-1}$  is the Stokes constant,  $\rho_l$  is the density of liquid water,  $N$  is the droplet number concentration,  $L$  is the liquid-water content,  $R_{3c}$  is a prescribed critical droplet radius, and  $R_3$  is the volume-weighted mean radius. ( $R_p$  is the mean radius of the  $p$ th moment of the droplet-size distribution, defined by  $R_p = (\int R^p n(R) dR / N)^{1/p}$ , where  $n(R) dR$  is the number concentration of droplets with radii between  $R$  and  $R + dR$ .) The Heaviside function  $H(R_3 - R_{3c})$  suppresses autoconversion unless  $R_3$  exceeds  $R_{3c}$ . The critical radius is usually "tuned" in GCMs to obtain a realistic simulation; values between 4.5 and 10  $\mu\text{m}$  have been adopted.  $E_c$  is typically assumed to equal 0.55, but several authors have argued that this value is much too large [Baker, 1993; Austin et al., 1995; Khairoutdinov and Kogan, 2000].

[6] However, this scheme does not account for the dispersion effect, and also employs the unrealistic assump-

tion of constant collection efficiency. A new autoconversion parameterization (“ $R_6$  scheme”), which removes these limitations, is [Liu and Daum, 2004; Liu et al., 2004]

$$P = \left( \frac{3}{4\pi\rho_l} \right)^2 \frac{\kappa_2 \beta_6^6}{N} L^3 H(R_6 - R_{6c}), \quad (2)$$

where  $R_6$  is the mean radius of the sixth moment of the droplet size distribution, and  $\kappa_2 = 1.9 \times 10^{11} \text{ cm}^3 \text{ s}^{-1}$  is a constant from the Long collection kernel, which represents the increase of collection efficiency with increasing collector drop size. The dispersion effect is described by  $\beta_6 = R_6/R_3$ , where, assuming a gamma distribution for the cloud-droplet spectrum,

$$\beta_6 = \left[ \frac{(1+3\epsilon^2)(1+4\epsilon^2)(1+5\epsilon^2)}{(1+\epsilon^2)(1+2\epsilon^2)} \right]^{1/6}, \quad (3)$$

where  $\epsilon$  is the relative dispersion of the droplet size distribution (ratio of the standard deviation to the mean radius). Instead of using a fixed critical radius,  $R_{6c}$  was derived as a function of  $L$  and  $N$  by Liu et al. [2004] as

$$R_{6c} = 4.09 \times 10^{-4} \beta_{\text{con}}^{1/6} \frac{N^{1/6}}{L^{1/3}}, \quad (4)$$

where  $R_{6c}$  is in  $\mu\text{m}$ ,  $L$  in  $\text{g m}^{-3}$ ,  $N$  in  $\text{cm}^{-3}$  and  $\beta_{\text{con}} = 1.15 \times 10^{23} \text{ s}^{-1}$  is the mean value of the condensation rate constant. Due to scatter in the measurements, there is considerable uncertainty in  $\beta_{\text{con}}$ , and hence in  $R_{6c}$ . A parameterization for the relative dispersion is [Rotstaysn and Liu, 2003]

$$\epsilon = 1 - 0.7 \exp(-\alpha N), \quad (5)$$

where  $\alpha = 0.003$  gave a good fit to the data, although the presence of considerable scatter was noted.

[7] In a GCM, the critical droplet radius is used to calculate  $L_c$ , the critical liquid-water content for the onset of autoconversion. In the  $R_3$  scheme,  $L_c$  is trivially obtained as

$$L_c = \frac{4\pi\rho_l}{3} R_{3c}^3 N. \quad (6)$$

When using the  $R_6$  scheme,  $R_{6c}$  is parameterized using equation (4). Then, use of  $R_{3c} = R_{6c}/\beta_6$  and equation (6) gives

$$L_c = \frac{4\pi\rho_l}{3L} \left( \frac{4.09 \times 10^{-4} \beta_{\text{con}}^{1/6} N^{1/2}}{\beta_6} \right)^3. \quad (7)$$

At the critical point,  $L = L_c$ , so a unique expression for  $L_c$  in terms of  $N$  can be obtained by setting  $L = L_c$  in equation (7) and solving for  $L_c$ .

### 3. Model and Experiments

[8] To quantify the impact of the  $R_6$  scheme on the second indirect effect, we used the CSIRO Mark3 GCM [Gordon et al., 2002] at low resolution (spectral R21). The model has been updated by treatments of the tropospheric

**Table 1.** Global-Mean Cloud Liquid-Water Path (LWP) and Top-of-Atmosphere Shortwave Cloud Forcing (SCF) From Each Simulation, and the Difference in Net Cloud Radiative Forcing (ACF) Between the PD and PI Simulations of Each Pair<sup>a</sup>

	R3AUTO		R6C R3RATE		R6AUTO	
	PD	PI	PD	PI	PD	PI
LWP	58.02	55.01	57.86	55.47	63.56	62.14
SCF	-49.22	-48.39	-49.25	-48.63	-50.88	-50.56
ΔCF	-0.71		-0.52		-0.28	

<sup>a</sup>LWP in  $\text{g m}^{-2}$ ; SCF and ΔCF in  $\text{W m}^{-2}$ .

sulfur cycle [Rotstaysn and Lohmann, 2002] and carbonaceous aerosols (based on Cooke and Wilson [1996]). Sea-salt aerosol in the marine boundary layer is diagnosed as a function of windspeed [O’Dowd et al., 1997]. The present-day (PD) emissions are applicable to the 1980s, and follow Rotstaysn and Lohmann [2002] for the sulfur emissions, and IPCC [2001b] for the carbonaceous aerosols. Preindustrial (PI) emissions are obtained by setting the industrial emissions to zero, and the biomass-burning emissions to 10% of the PD values.

[9] The model includes a detailed cloud microphysical scheme [Rotstaysn, 1997; Rotstaysn and Liu, 2003].  $N$  as used to calculate autoconversion is estimated empirically from the mass concentrations of sulfate, organic matter and sea-salt aerosol [Menon et al., 2002]. A minimum value of  $N = 20 \text{ cm}^{-3}$  is applied, and there are no effects of aerosols on convective clouds or ice clouds.

[10] We performed three (PD and PI) pairs of simulations, to identify the effect of using the  $R_6$  scheme (equations (2) and (7)) instead of the  $R_3$  scheme (equations (1) and (6)):

[11] 1. R3AUTO: Autoconversion is calculated using the  $R_3$  scheme for the autoconversion rate and threshold, with  $R_{3c} = 7.5 \mu\text{m}$ .

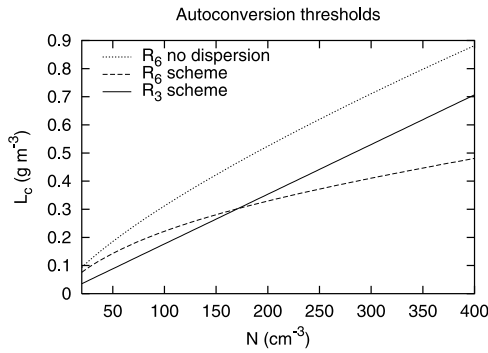
[12] 2. R6C R3RATE: The autoconversion rate follows the  $R_3$  scheme, but the threshold follows the  $R_6$  scheme.

[13] 3. R6AUTO: Both the autoconversion rate and threshold follow the  $R_6$  scheme.

[14] To suppress the first indirect effect,  $N$  as used to calculate the droplet effective radius in the radiation scheme was prescribed as  $300 \text{ cm}^{-3}$  over land and  $100 \text{ cm}^{-3}$  over oceans. No direct aerosol effects were allowed, and the concentration of  $\text{CO}_2$  was held fixed at 345 ppm. We ran the model for 21 years with prescribed, monthly mean sea-surface temperatures. The first year of each simulation was discarded as a “spinup” period, and statistics were obtained from the remaining 20 years.

### 4. Results and Discussion

[15] Table 1 summarizes the results from the three pairs of simulations. First, note that the  $R_6$  scheme gives reasonable global-mean values of shortwave cloud forcing (SCF) and liquid-water path (LWP) without any retuning of the model. This needs further investigation, since we did not explicitly consider the effects of subgrid variability in cloud-water content [e.g., Rotstaysn, 2000]. The difference in net cloud forcing (ΔCF) between the PD and PI runs gives an estimate of the second indirect aerosol effect, including the small longwave component. The second indirect effect is about 61% smaller in the R6AUTO runs ( $-0.28 \text{ W m}^{-2}$ ) com-



**Figure 1.** Autoconversion thresholds given by the  $R_3$  scheme with  $R_{3c} = 7.5 \mu\text{m}$ , and by the  $R_6$  scheme with and without the dispersion effect. See color version of this figure in the HTML.

pared to the R3AUTO runs ( $-0.71 \text{ W m}^{-2}$ ). The value from the R6C\_R3RATE run lies in between the other two, showing that the  $R_6$  schemes for the autoconversion rate and threshold both act to reduce the second indirect effect in our model. For each pair of simulations, the difference in LWP is qualitatively consistent with the difference in SCF.

[16] To explain why the  $R_6$  threshold gives a smaller second indirect effect than the  $R_3$  threshold, Figure 1 shows  $L_c$  versus  $N$  for the  $R_3$  scheme (equation (6)) and the  $R_6$  scheme (equation (7)). Without the dispersion effect ( $\beta_6 = 1$ ), the  $R_6$  scheme gives a stronger increase of  $L_c$  with  $N$  than the  $R_3$  scheme, because  $R_{6c}$  increases with  $N$  (equation (4)) instead of being fixed. Inclusion of the dispersion effect in the  $R_6$  scheme (equations (3) and (5)) reduces the slope of the  $L_c$  versus  $N$  curve. Compared to the  $R_3$  scheme, the  $R_6$  scheme with dispersion gives larger  $L_c$  for small  $N$  and smaller  $L_c$  for large  $N$ , and thus gives a smaller second indirect effect.

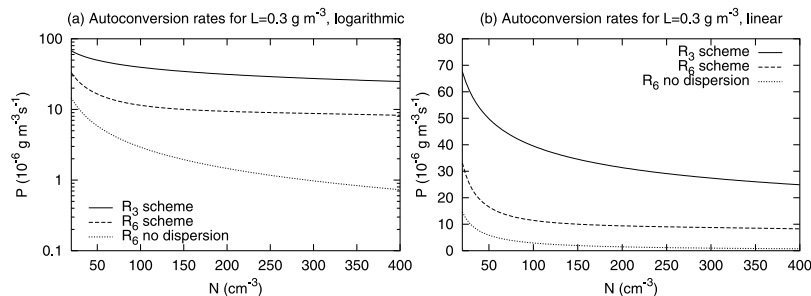
[17] To understand why the  $R_6$  rate gives a smaller second indirect effect than the  $R_3$  rate, we plot the autoconversion rates versus  $N$  for  $L = 0.3 \text{ g m}^{-3}$  in Figure 2. Figure 2a uses a logarithmic scale for the vertical axis, so that the slope ( $d \log P / dN$ ) shows the relative changes of  $P$ . The autoconversion rate is smaller in the  $R_6$  scheme than in the  $R_3$  scheme (and even more so without the dispersion effect). This explains why R6AUTO has larger values of LWP than R6C\_R3RATE. Without the dispersion effect, the steeper decrease of  $P$  with  $N$  in the  $R_6$  scheme ( $N^{-1}$ ) compared to the  $R_3$  scheme ( $N^{-1/3}$ ) is evident. Inclusion of the dispersion effect in the  $R_6$  scheme brings the slope of

the  $P$  versus  $N$  curve closer to that of the  $R_3$  scheme, though it is still steeper for small values of  $N$ .

[18] However, an important point is that the magnitude of the second indirect effect depends on absolute changes of  $P$  with  $N$ , as shown by the slopes of the curves in Figure 2b, which uses a linear scale. Inclusion of the dispersion effect in the  $R_6$  scheme markedly increases  $P$ , but only slightly increases the decrease of  $P$  with  $N$ . Since  $P$  is much smaller in the  $R_6$  scheme than in the  $R_3$  scheme, the decrease of  $P$  with  $N$  is also smaller. (If  $P \propto N^{-\gamma}$ , then  $dP/dN = -\gamma P N^{-1}$ , where  $\gamma = 1/3$  in the  $R_3$  scheme and  $\gamma = 1$  in the  $R_6$  scheme without the dispersion effect. Figure 2b shows that, without the dispersion effect,  $P$  is more than 3 times smaller in the  $R_6$  scheme than in the  $R_3$  scheme, so  $dP/dN$  is also smaller. The dispersion effect modifies the above by increasing  $P$  and decreasing the effective value of  $\gamma$ . The net dispersion effect depends on the competition between these two effects; the slopes of the two lower curves in Figure 2b show that they roughly balance for large  $N$ , and the effect of increased  $P$  is stronger for small  $N$ .)

[19] Previous indications that the autoconversion rate given by the  $R_3$  scheme is too large [Baker, 1993; Austin et al., 1995; Delobbe and Gallée, 1998] suggest that the lower autoconversion rate in the  $R_6$  scheme is more realistic. Recently, R. Wood (preprint, 2004, available at <http://www.atmos.washington.edu/~robwood/papers/drzipa1b.pdf>) found that the  $R_6$  scheme and the Khairoutdinov and Kogan [2000] scheme were much more accurate than the  $R_3$  scheme, which strongly overestimated autoconversion. However, Menon et al. [2003] found that the  $R_3$  scheme “severely underestimated” precipitation, so further work is needed to reconcile these differences.

[20] We also performed some sensitivity tests. First, we repeated the R6AUTO runs with the dispersion effect turned off in the autoconversion rate (i.e., we set  $\beta_6 = 1$  in equation (2)). This test gave  $\Delta\text{CF} = -0.22 \text{ W m}^{-2}$ , a little smaller than the result from the R6AUTO run. This is consistent with the middle curve in Figure 2b having a slightly steeper average slope than the lowest curve. It further underlines that the absolute changes of  $P$  with  $N$  control the simulated second indirect effect, rather than the relative changes as described by the functional variation of  $P$  with  $N$ . Note that  $\beta_6 = 1$  is the assumption that is usually made in the  $R_3$  scheme, but it is equally valid to choose a larger value of  $\beta_6$  to represent a droplet spectrum with fixed relative dispersion. A larger value of  $\beta_6$  would give a larger autoconversion rate, and hence a larger second indirect effect. Next, we repeated R3AUTO and R6AUTO with  $N$



**Figure 2.** Autoconversion rates for  $L = 0.3 \text{ g m}^{-3}$  given by the  $R_3$  scheme, and by the  $R_6$  scheme with and without the dispersion effect, using (a) logarithmic and (b) linear scales. See color version of this figure in the HTML.



allowed to vary in the radiation scheme as well as in the autoconversion scheme, to estimate the total indirect aerosol effect on liquid-water clouds. As above, the dispersion effect was included in the parameterization of effective radius [Rotstayn and Liu, 2003]. We obtained  $\Delta CF = -1.63 \text{ W m}^{-2}$  using the  $R_3$  scheme, and  $-1.09 \text{ W m}^{-2}$  using the  $R_6$  scheme. The difference ( $0.54 \text{ W m}^{-2}$ ) is close to the difference between our estimates for the second indirect effect ( $0.43 \text{ W m}^{-2}$ ).

[21] The results obtained with the  $R_6$  scheme are easier to reconcile with observations. For example,  $-1.09 \text{ W m}^{-2}$  for the total indirect aerosol effect is much closer to the estimate of  $-0.85 \text{ W m}^{-2}$  obtained when a GCM was constrained by satellite observations by Lohmann and Lesins [2002]. Also, the impact of the smaller autoconversion rate on the second indirect effect shows the importance of careful evaluation of autoconversion schemes and avoidance of artificial “tuning” of rates or thresholds.

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